



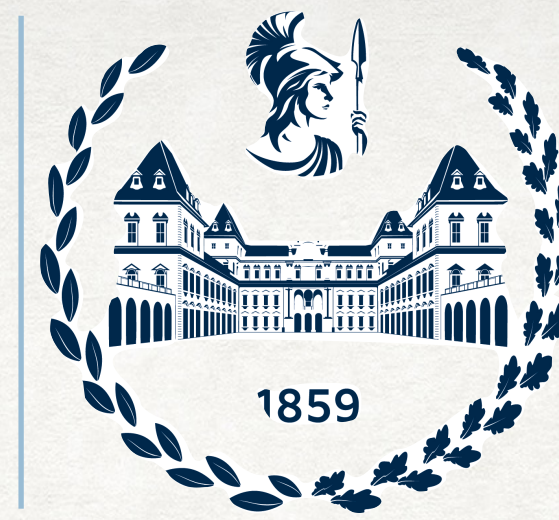
Ambient Sensing and
Processing Group



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DRIFT REJECTION FRONT-END FOR LONG-RANGE CAPACITIVE SENSORS FOR HUMAN INDOOR LOCALIZATION

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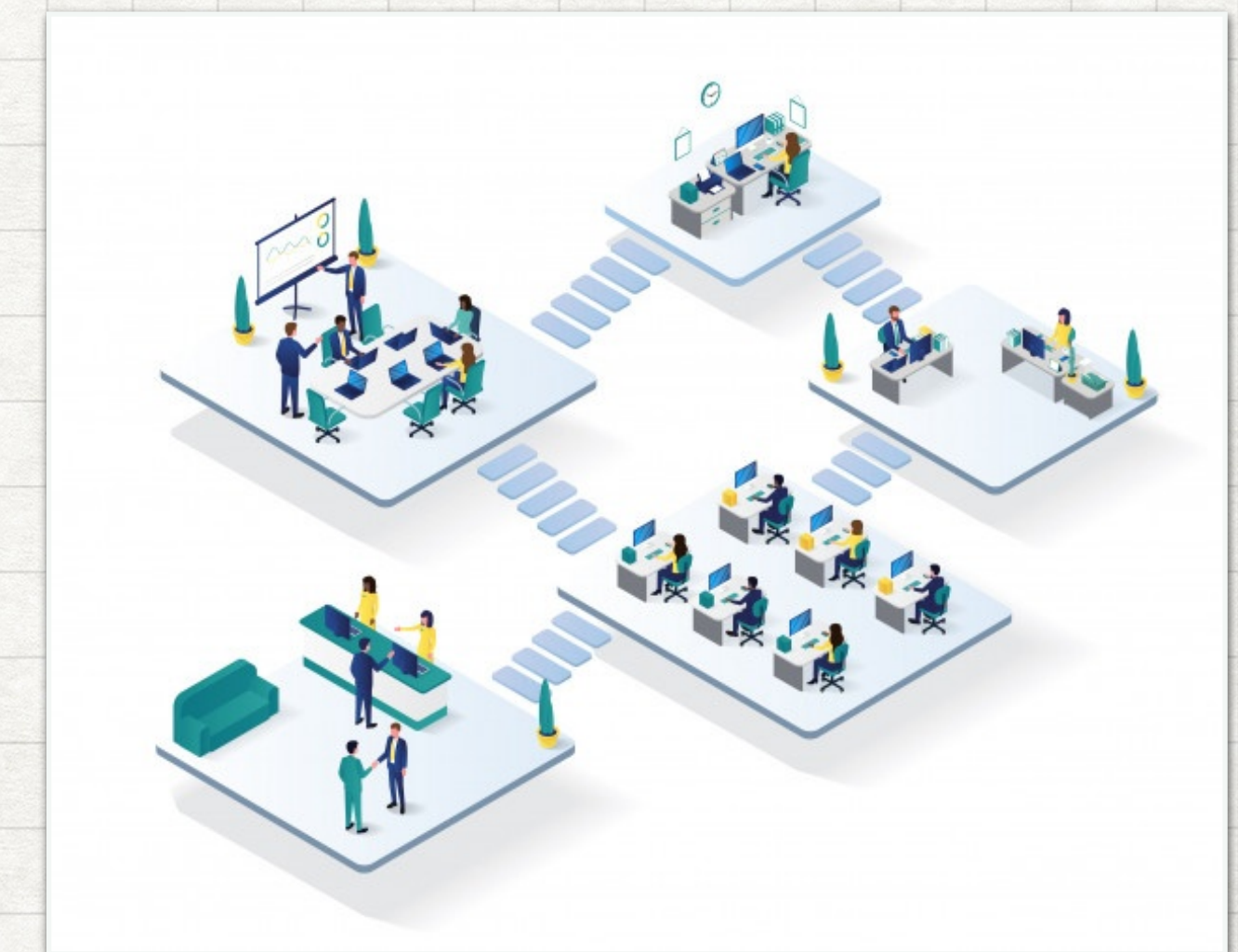
- Indoor Localization and Typical Application
- Capacitive sensors - Primer
- Main sources of noise
- Capacitive sensor front-ends
- Noise rejection results
- Conclusions



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INDOOR LOCALIZATION

- Monitor human activities to detect the early onset of diseases
- Assisted living for elderly people
- Detect unauthorized intrusions
- Home automation
- Reduce energy consumption





CAPACITIVE SENSORS - PRIMER

Capacitive sensors working in load mode:

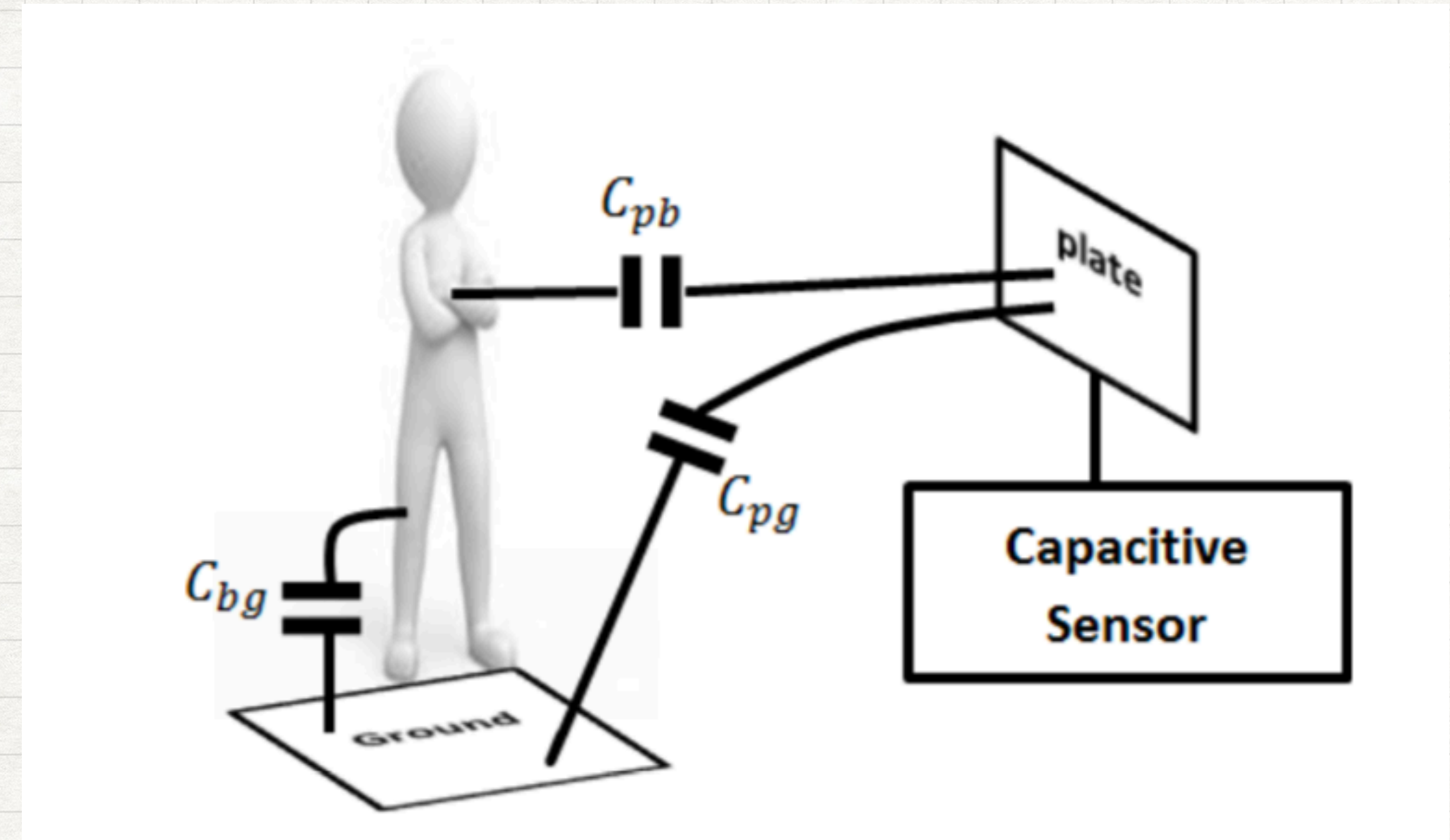
- One-plate transducer
- Human body as a constant-potential plate

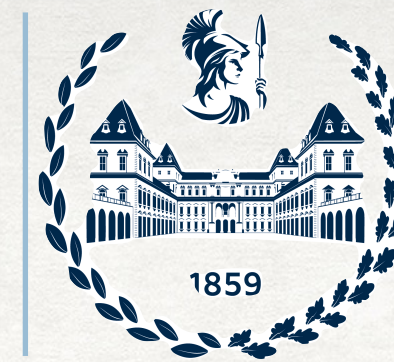
PROs

1. Privacy-aware
2. Low power
3. Low cost of installation
4. Tagless
5. Detection of conductive and non-conductive objects

CONs

1. Short sensing range
2. Electric and electromagnetic noise can limit accuracy



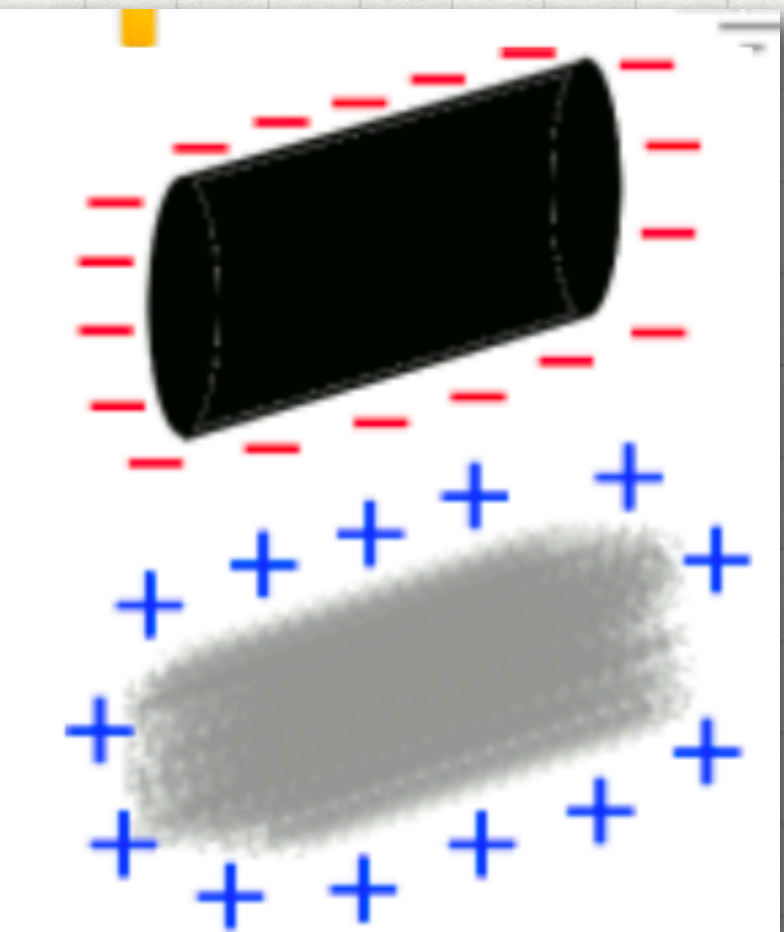
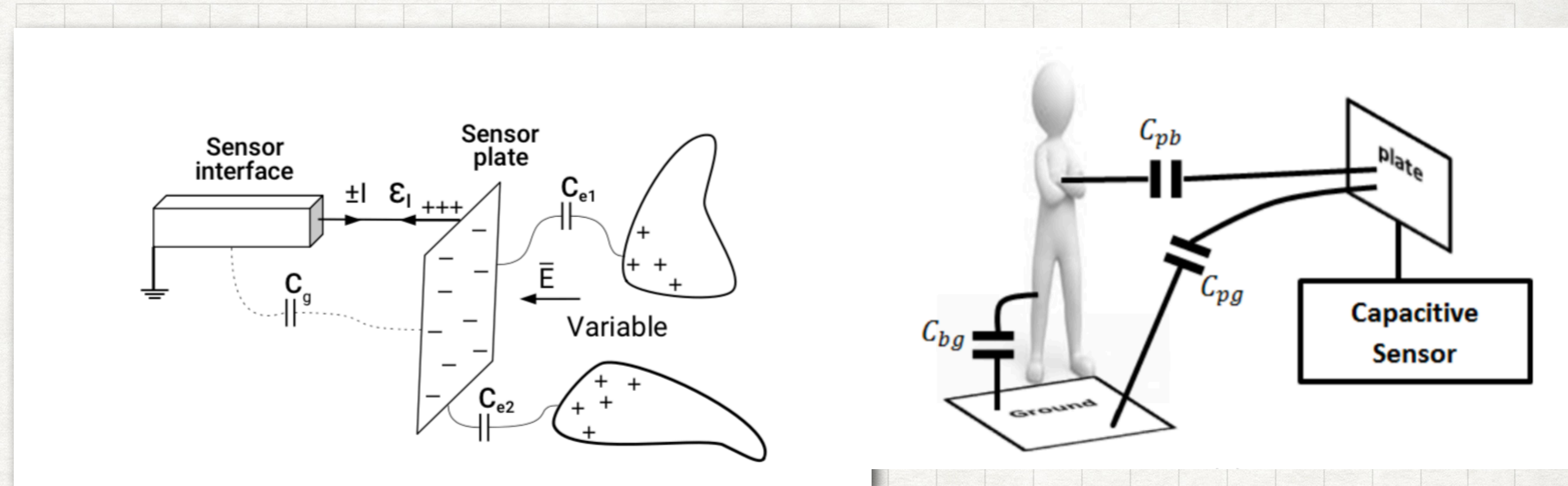


MAIN SOURCES OF NOISE

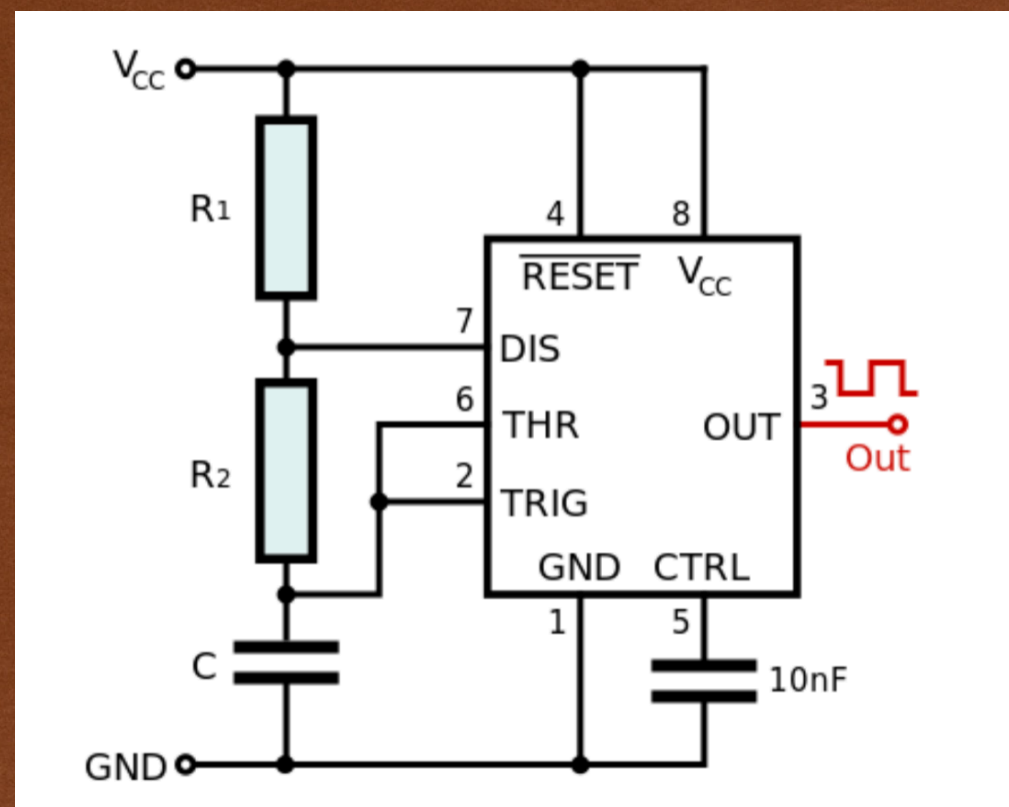
★ Low Frequency → Measurement Drift

- Environmental charge buildups → E variation → induced drift current ϵ_i → influence sensor interface parameters without a real change in sensor capacitance
- Actual capacitance changes → e.g. variable air humidity

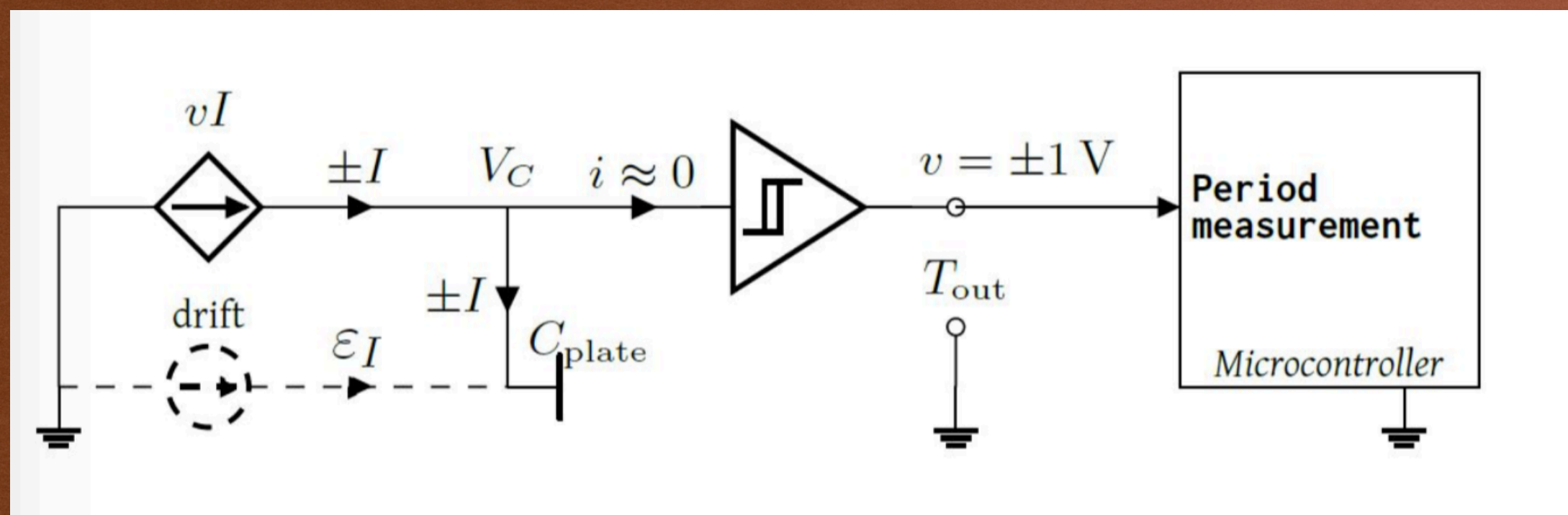
★ High Frequency → Measurement Jitter



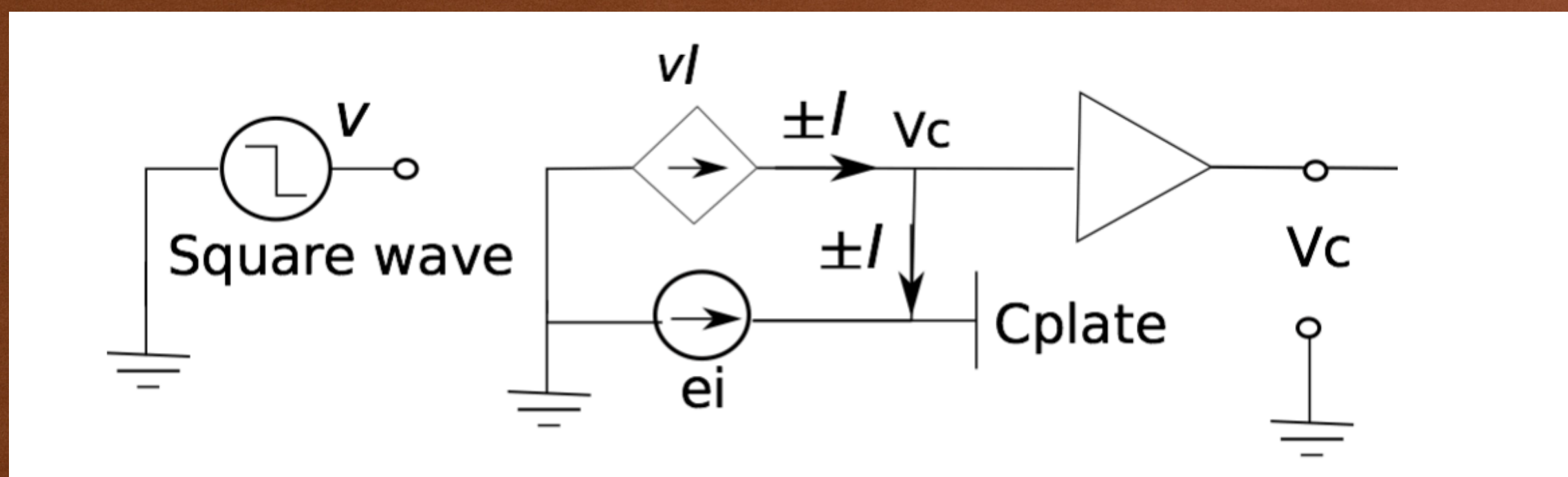
THREE ANALOG SIGNAL CONDITIONING CIRCUITRY



- RC-FE: period modulator, based on astable multivibrator



- IC-FE: period modulator, based on constant current charge-discharge

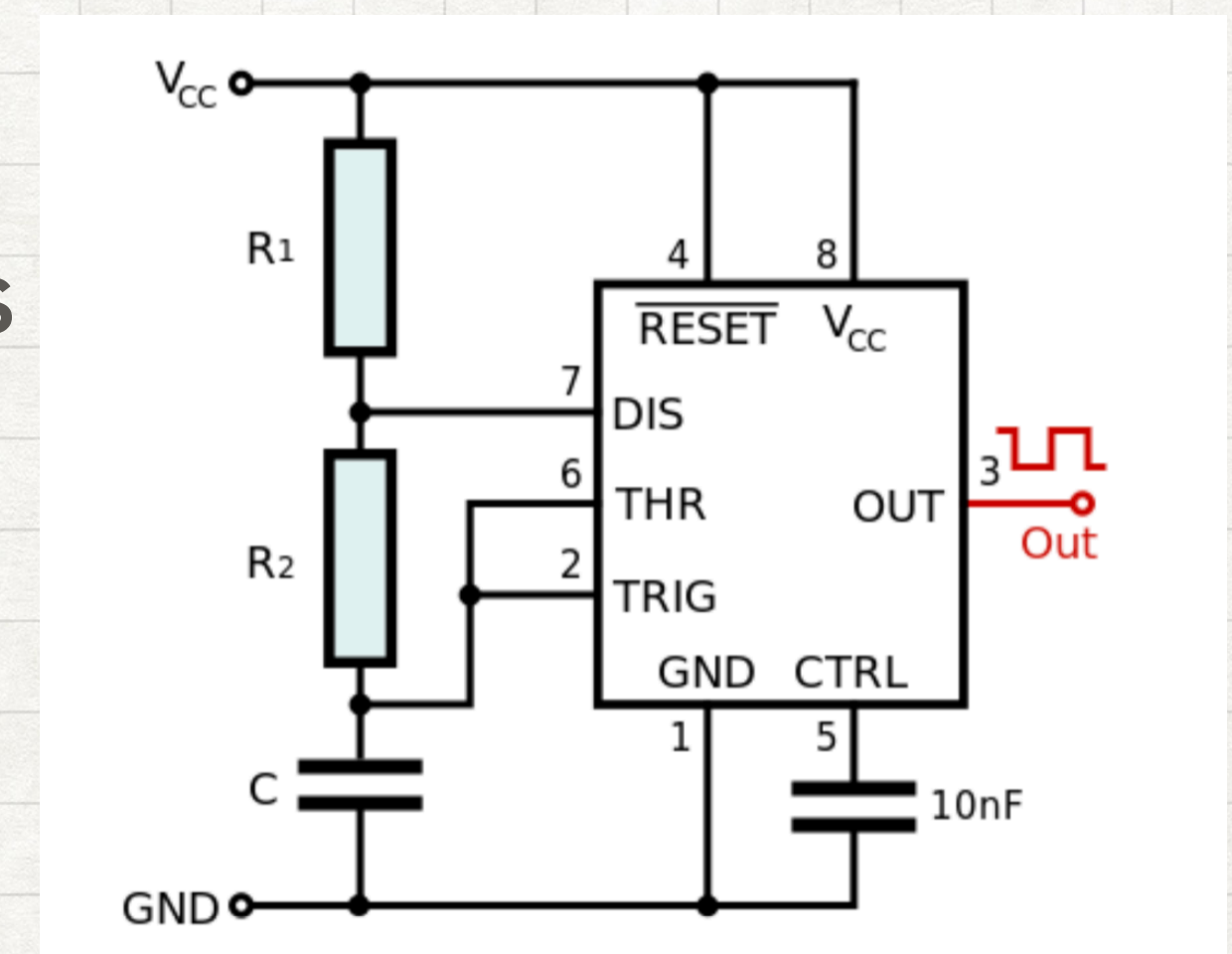


- IC-FE: slope modulator, based on constant current charge-discharge



RC PERIOD MODULATOR

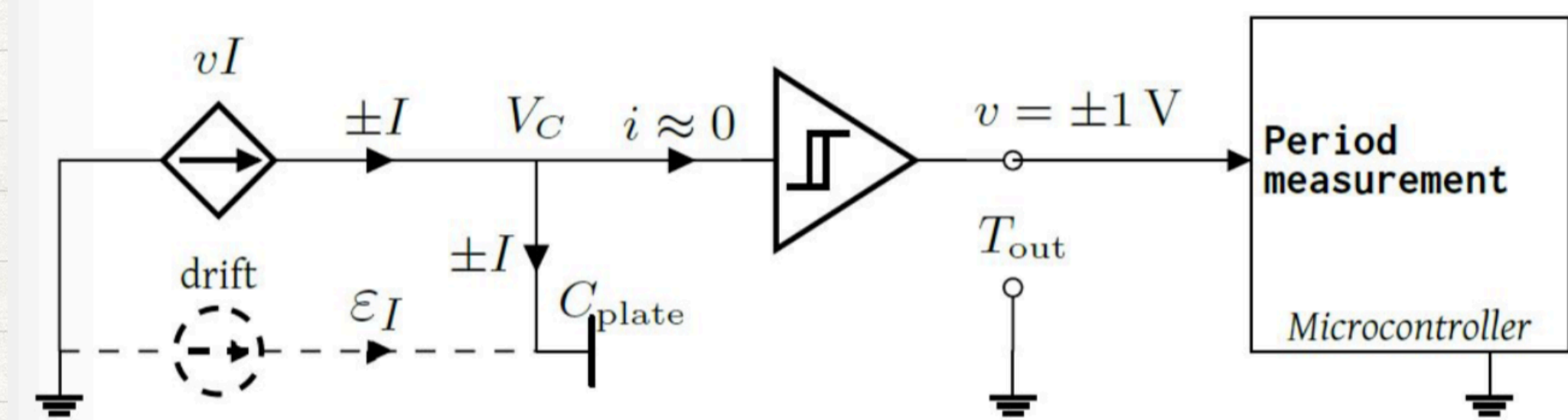
- ◆ astable oscillator
- ◆ RC-FE output is a square wave
- ◆ The period of the square wave depends on resistances value and capacitance value
- ◆ The two resistors are fixed





IC PERIOD MODULATOR

- ◆ It cyclically charges and discharges the plate using a voltage-controlled current source with constant current
- ◆ It uses a trigger of Schmitt with hysteresis thresholds
- ◆ As soon as the voltage triangular wave reaches one of the thresholds, the output of the trigger swings, consequently, the current source changes sign





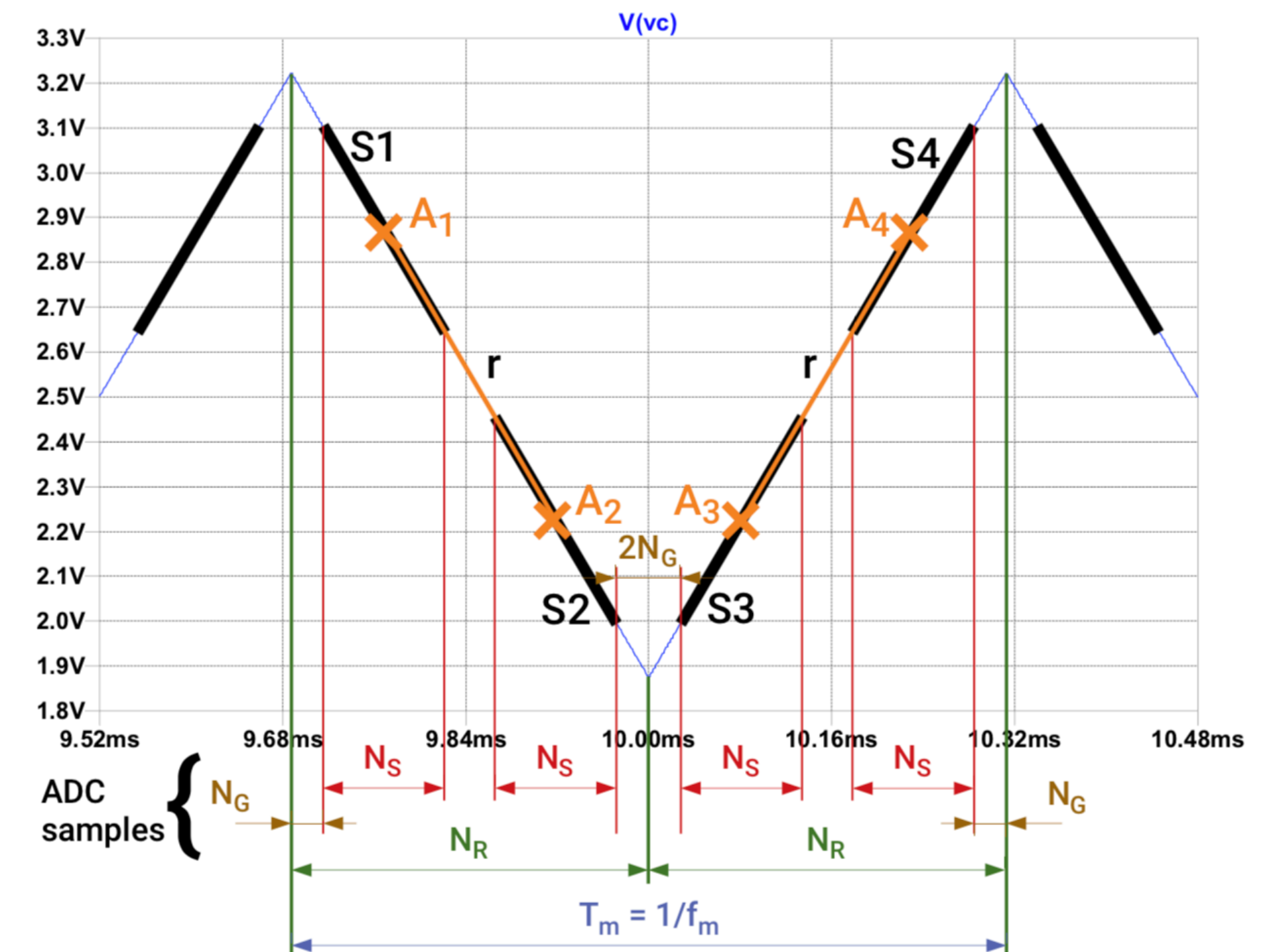
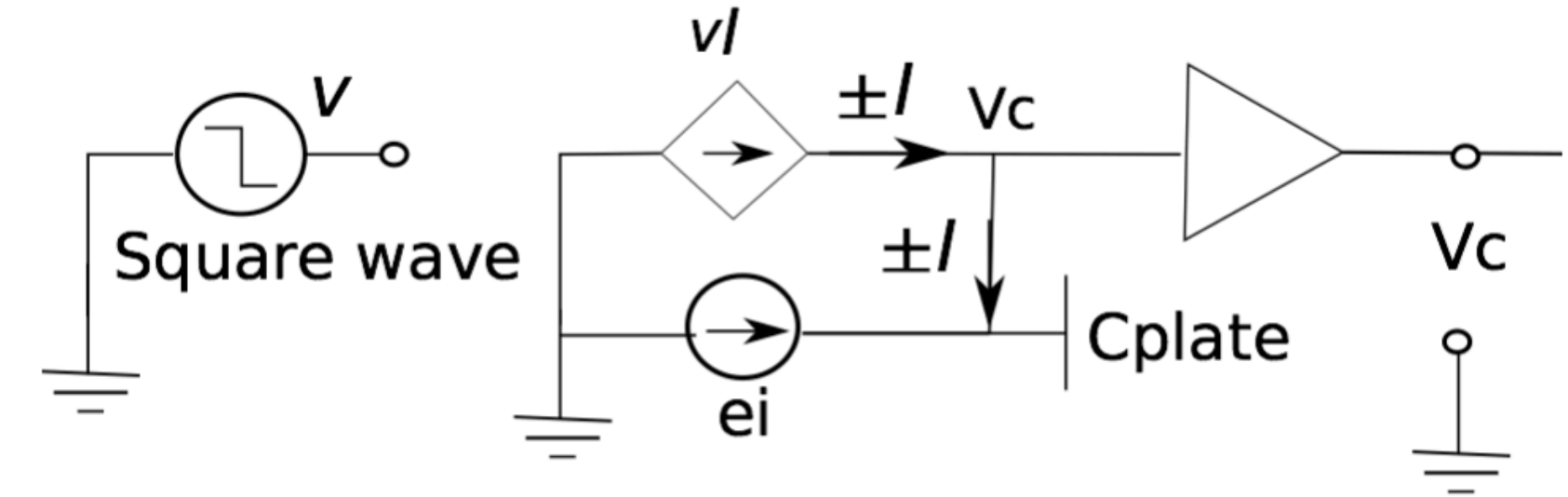
SLOPE MODULATOR

- ◆ Constant current that charges/discharges the plate, driven by a square wave
- ◆ Fixed charging/discharging time
- ◆ Plate voltage V_c is a triangular wave
- ◆ No pre-defined thresholds
- ◆ An Analog to Digital Converter is used to sample the plate voltage
- ◆ Digital calculation of two adjacent ramps with noise reduction
- ◆ Capacitance of the sensor is proportional to slope average

- $N_r=1000$
- $N_s=256$
- $N_g=243$
- $r=2$

Each segment is oversampled N_s time:

$N_s = 4^n$ (n additional accuracy bits after processing)



SLOPE MODULATOR CIRCUIT

PULSE 0V, 3.3V, 0.5ms, 1ms

VIN

Square wave generator

GND

R1
2.7k

R2
270
1.65V

OPA

LTC6082

R3
0

C1
470p

R4
2.7k

R5
27k
1.65V

R8
27k

OPB

LTC6082

R7
27k

FE_OUT

OPD

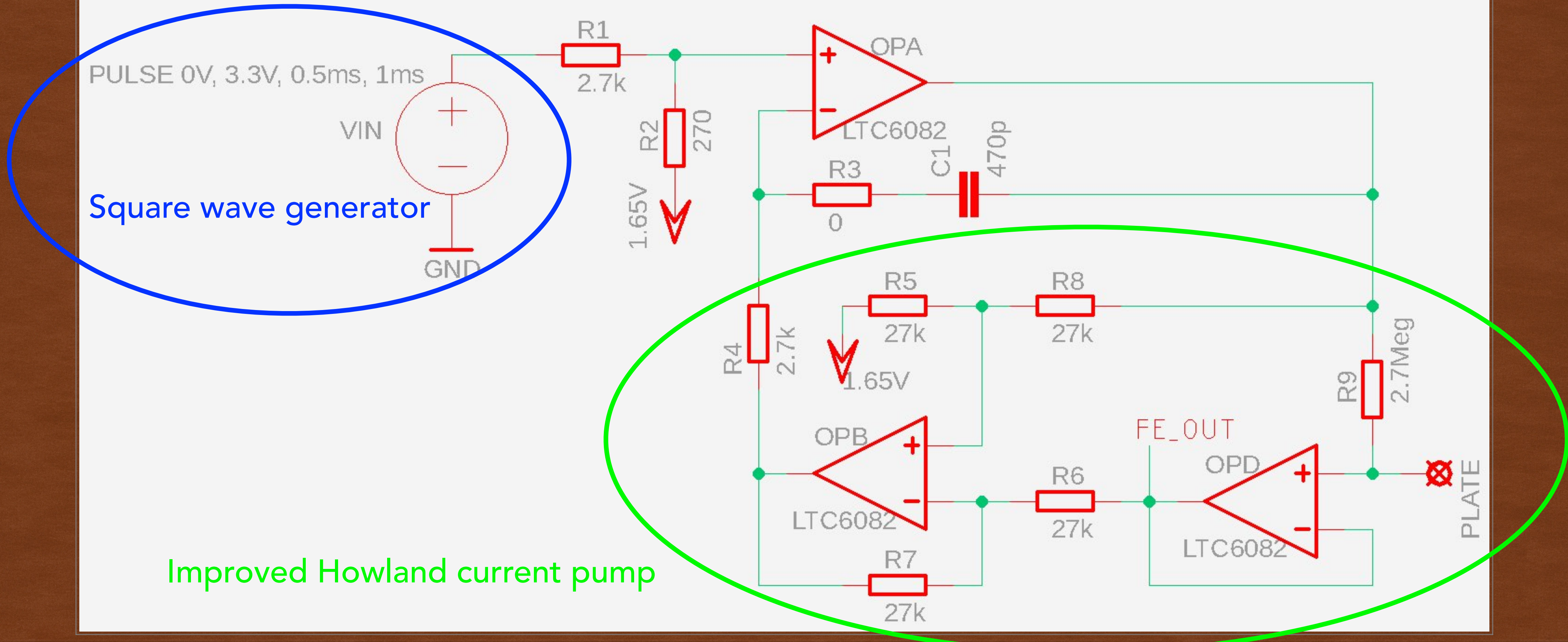
LTC6082

R6
27k

R9
2.7Meg

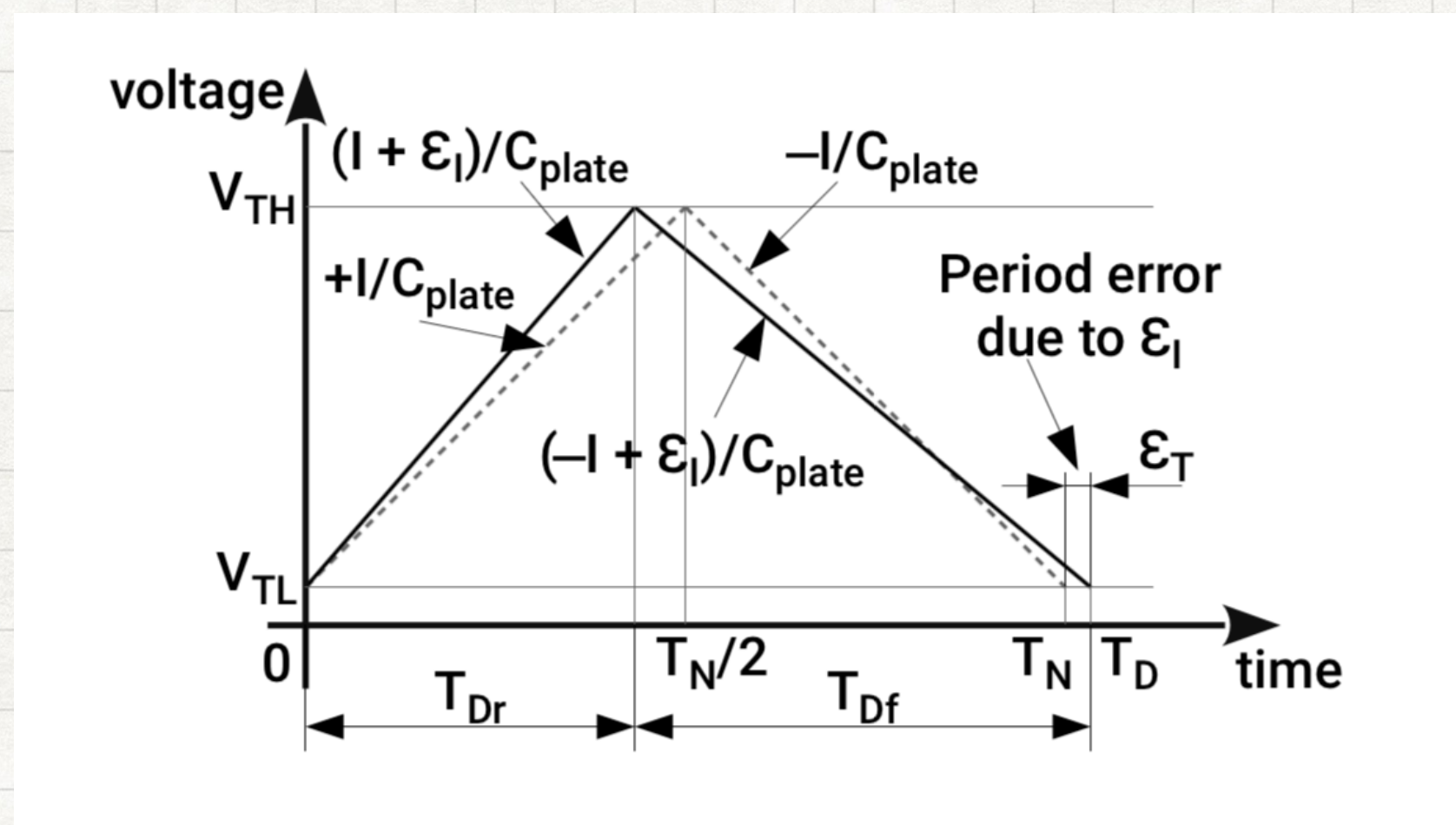
PLATE

Improved Howland current pump



PERIOD MODULATOR AND SLOPE MODULATOR MEASUREMENT TECHNIQUES AND QUASI-CONSTANT DRIFT CURRENT REJECTION

PERIOD MODULATOR

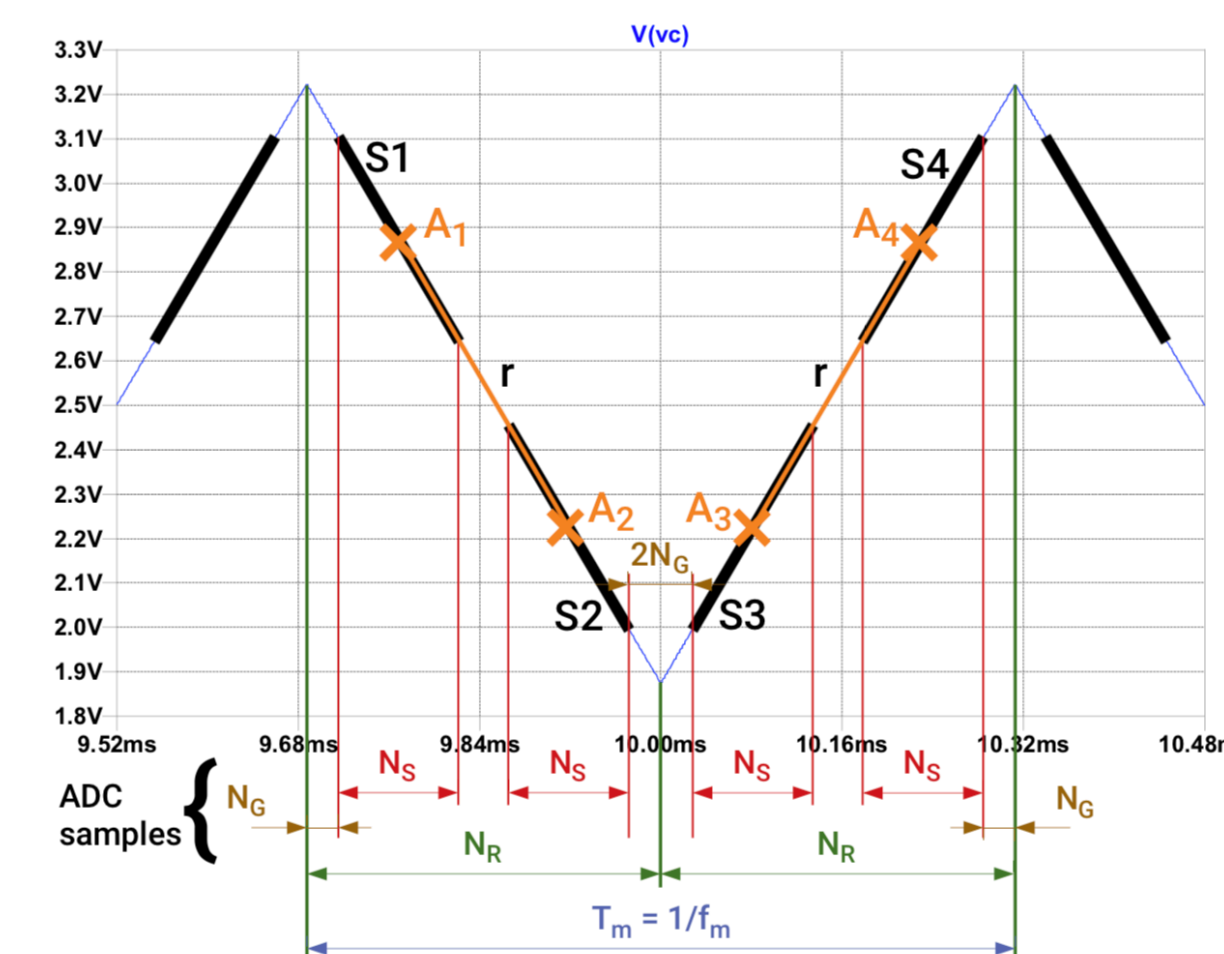


$$C_{plate} = \frac{I}{2(V_{TH} - V_{TL})} T_N.$$

$$T_{Dr} = C_{plate} \frac{V_{TH} - V_{TL}}{I + \epsilon_I}, \quad T_{Df} = C_{plate} \frac{V_{TL} - V_{TH}}{-I + \epsilon_I}$$

$$T_D = T_{Dr} + T_{Df} = \frac{2C_{plate} (V_{TH} - V_{TL}) I}{I^2 - \epsilon_I^2}$$

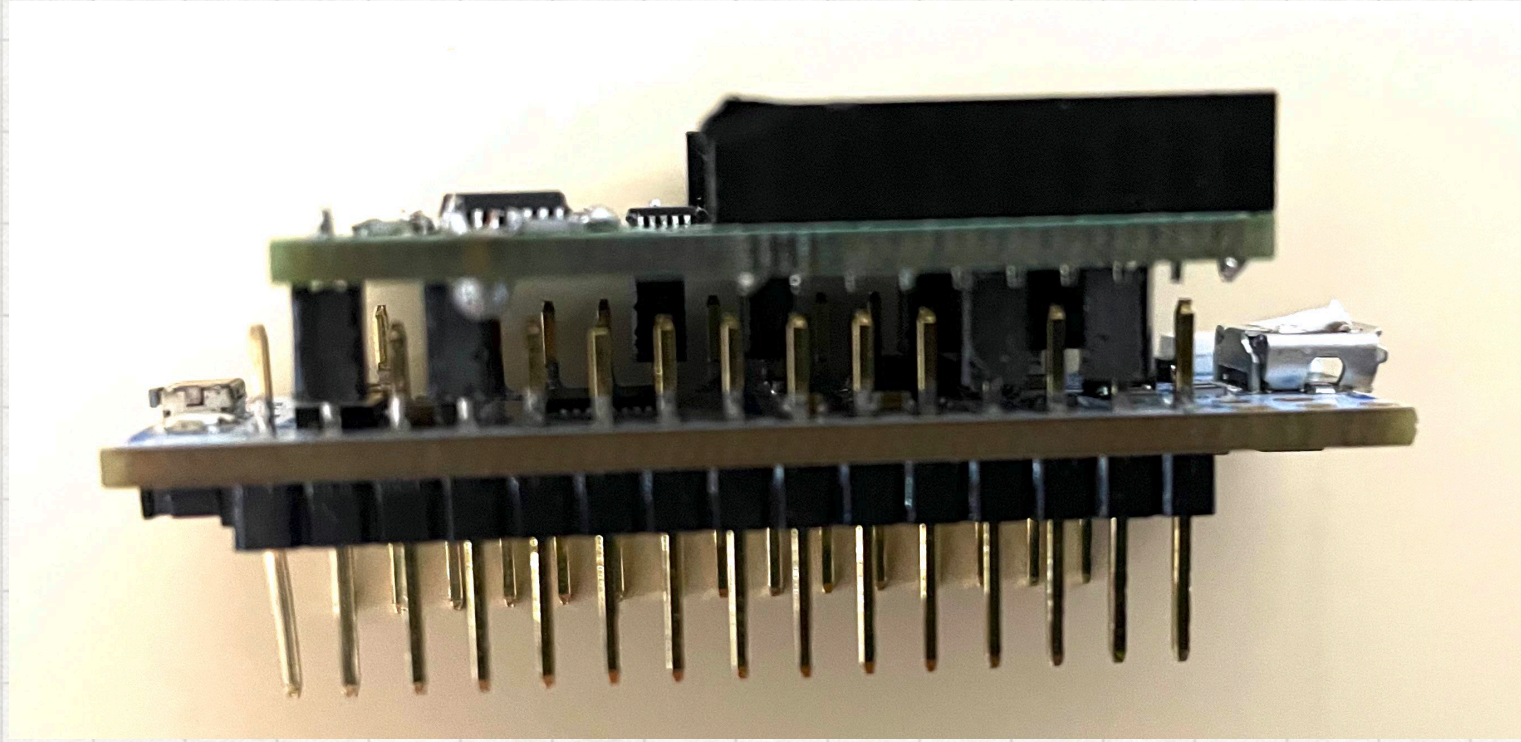
SLOPE MODULATOR



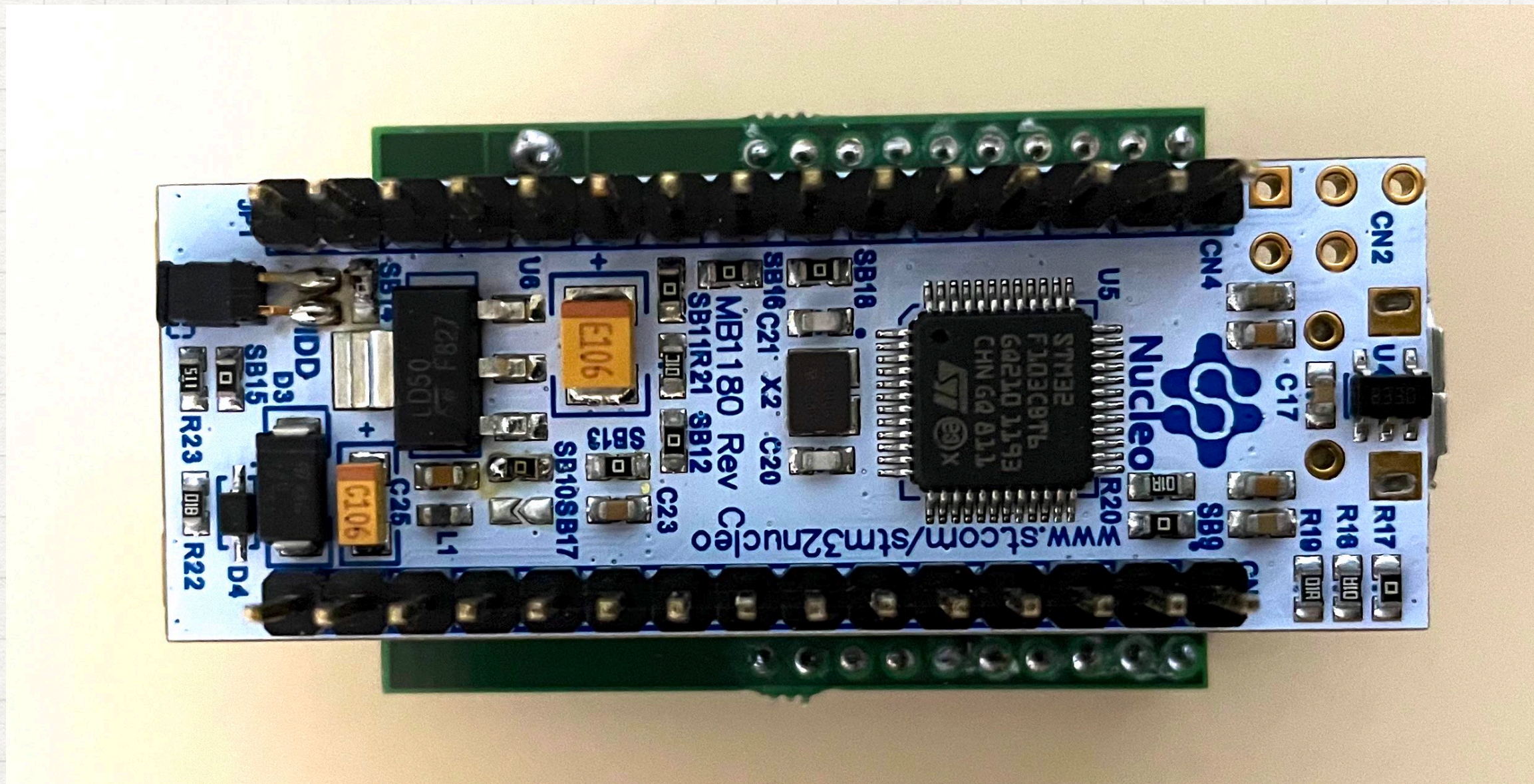
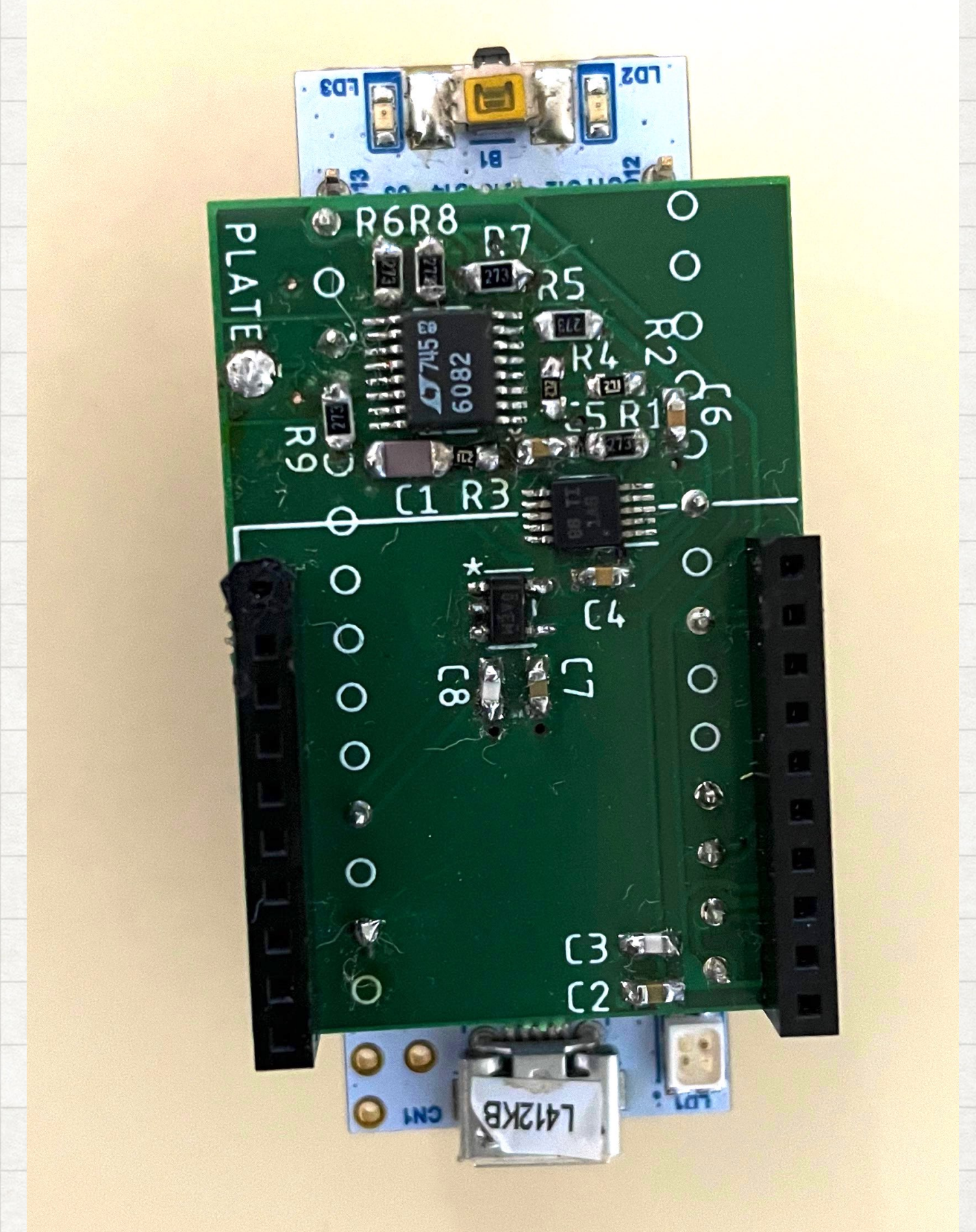
$$S = \frac{\Delta V_C}{\Delta t} = \frac{I}{C_{plate}}$$

$$S_r = \frac{I + \epsilon_I}{C_{plate}}, \quad S_f = \frac{-I + \epsilon_I}{C_{plate}}$$

$$S_a = \frac{|S_r| + |S_f|}{2} = \frac{1}{2} \left(\frac{I + \epsilon_I}{C_{plate}} - \frac{-I + \epsilon_I}{C_{plate}} \right) = \frac{I}{C_{plate}}$$



SLOPE MODULATOR PCB+ STM L412KB MICRO CONTROLLER





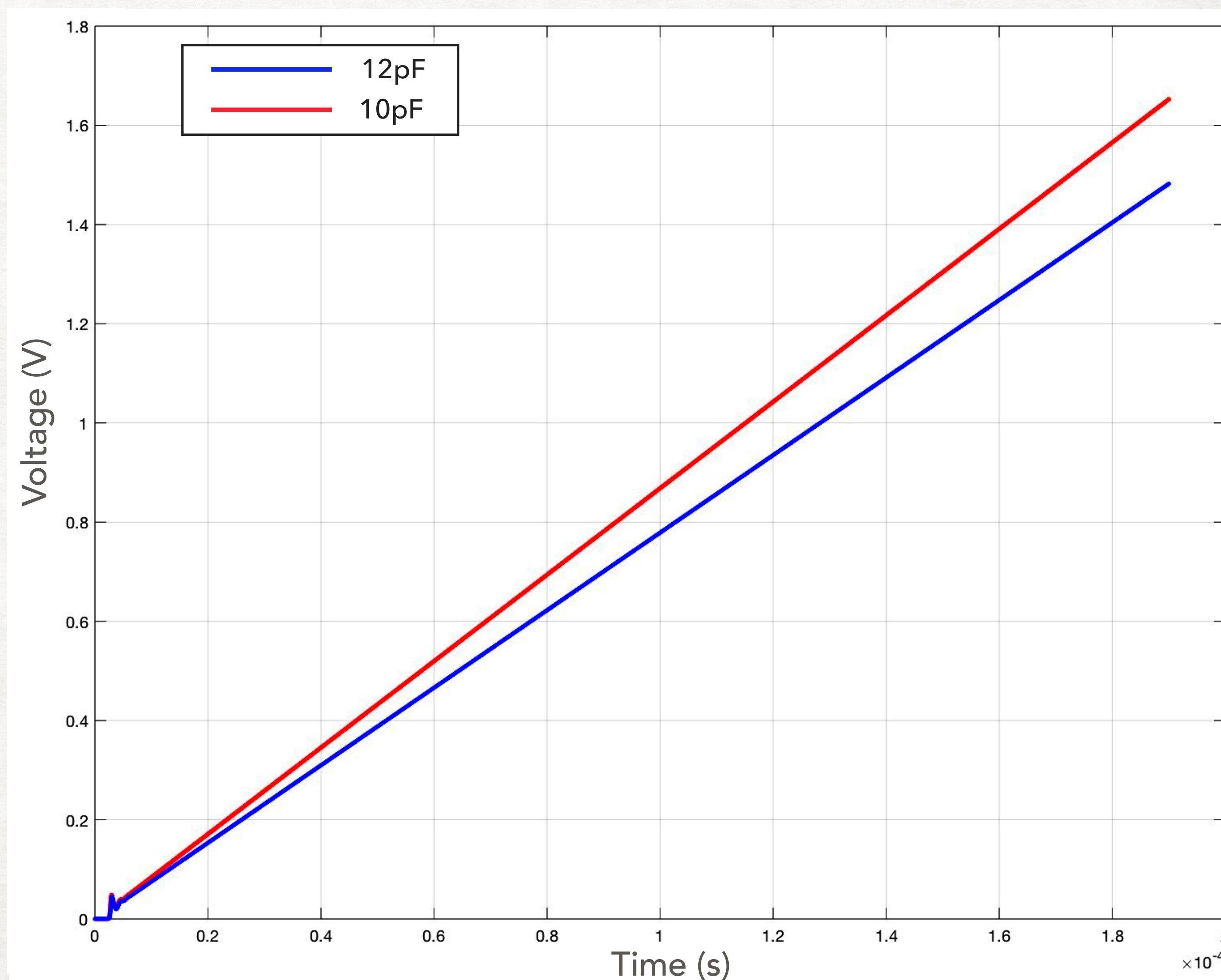
SENSITIVITY CHARACTERIZATION

Sensitivity as a variation of the output signal (slope), for small variation in the capacity of the plate.

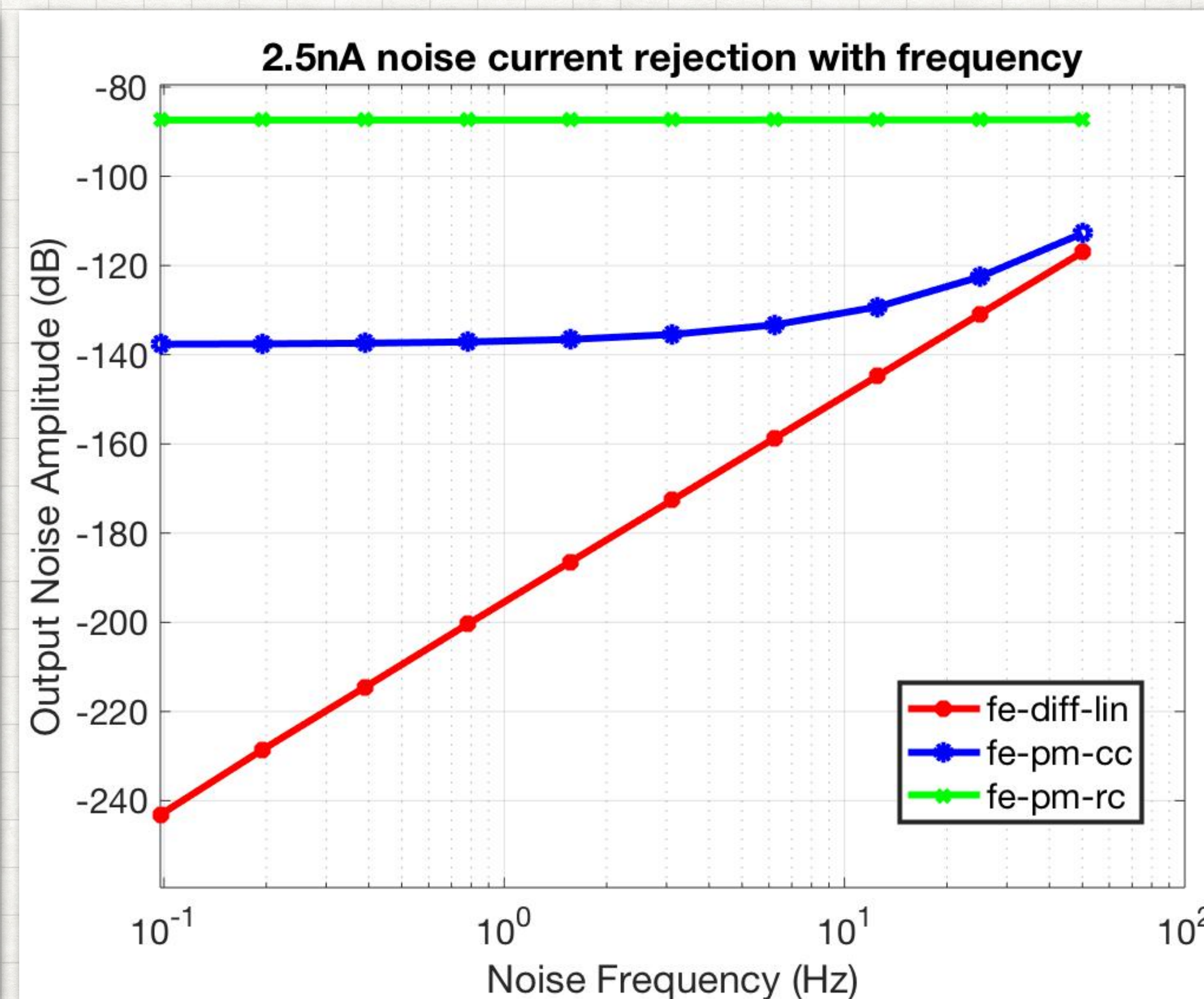
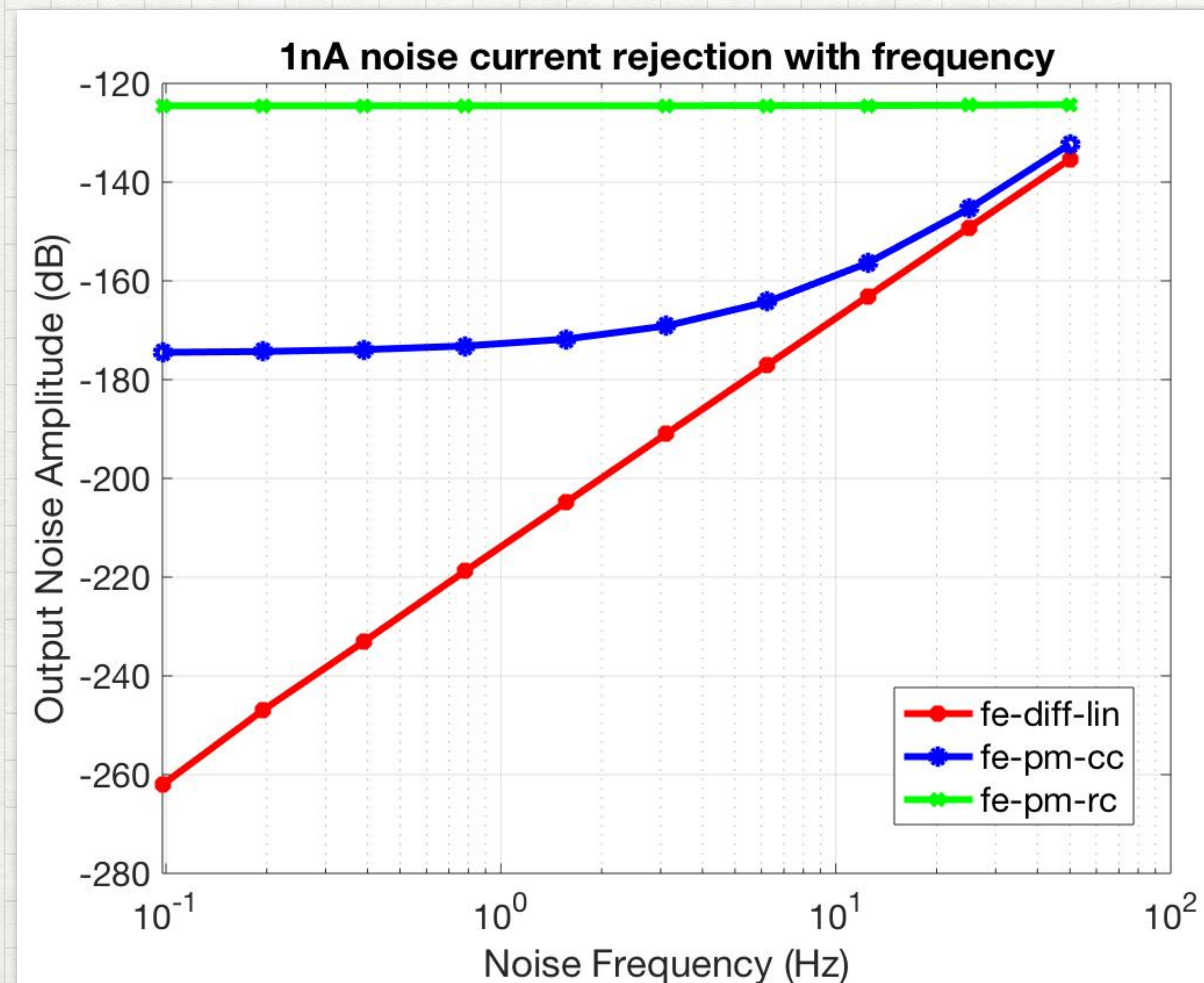
C	C'
10pF	12pF
S	S'
8697.0897V/s	7800.5667V/s

$$Srel \% = \frac{\frac{|S - S'|}{S}}{\frac{|C - C'|}{C}} \cdot 100$$

$$Srel \% = \frac{\frac{|8697.0897 - 7800.5667|}{8697.0897}}{\frac{|10 - 12|}{10}} \cdot 100 = 51 \%$$

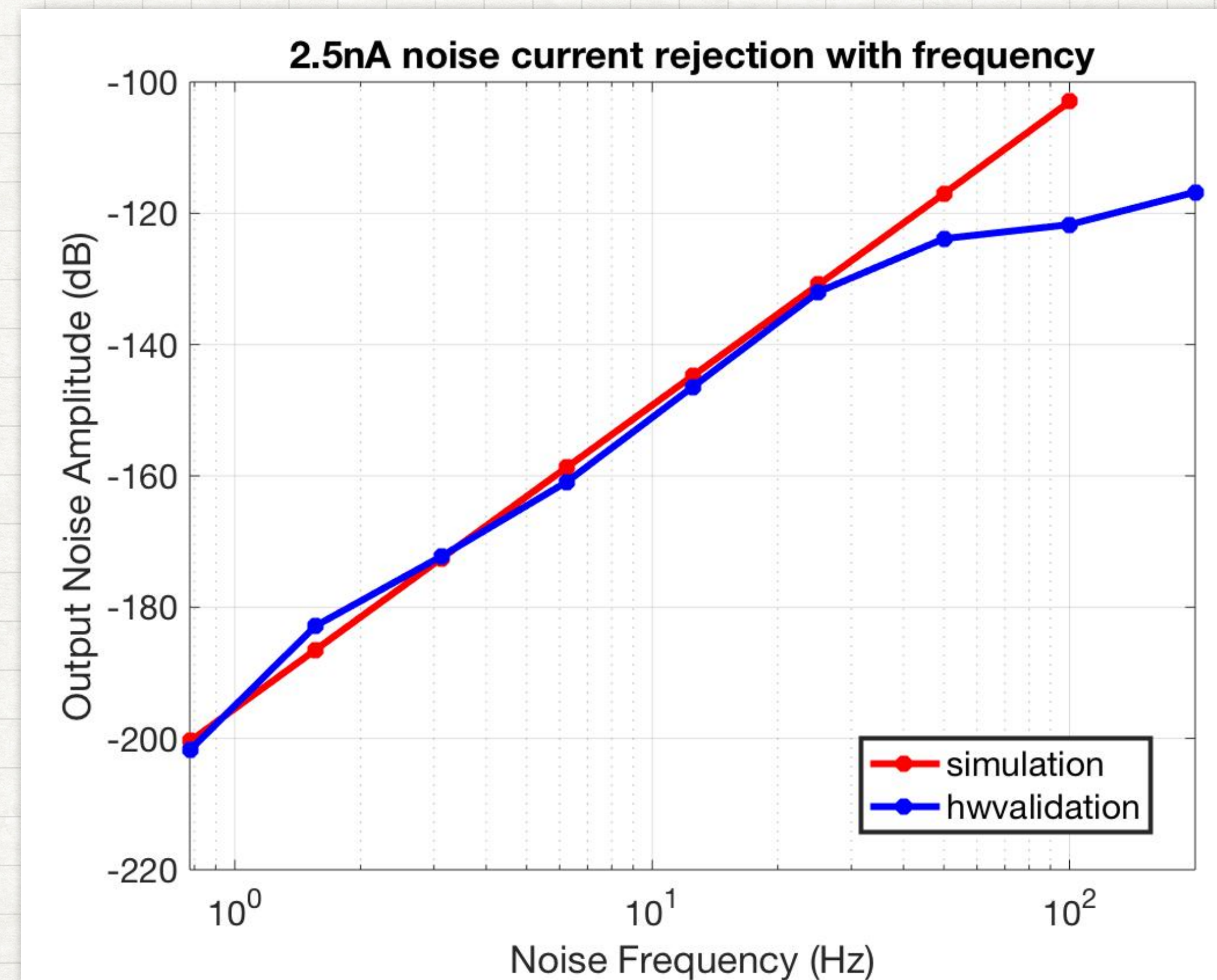
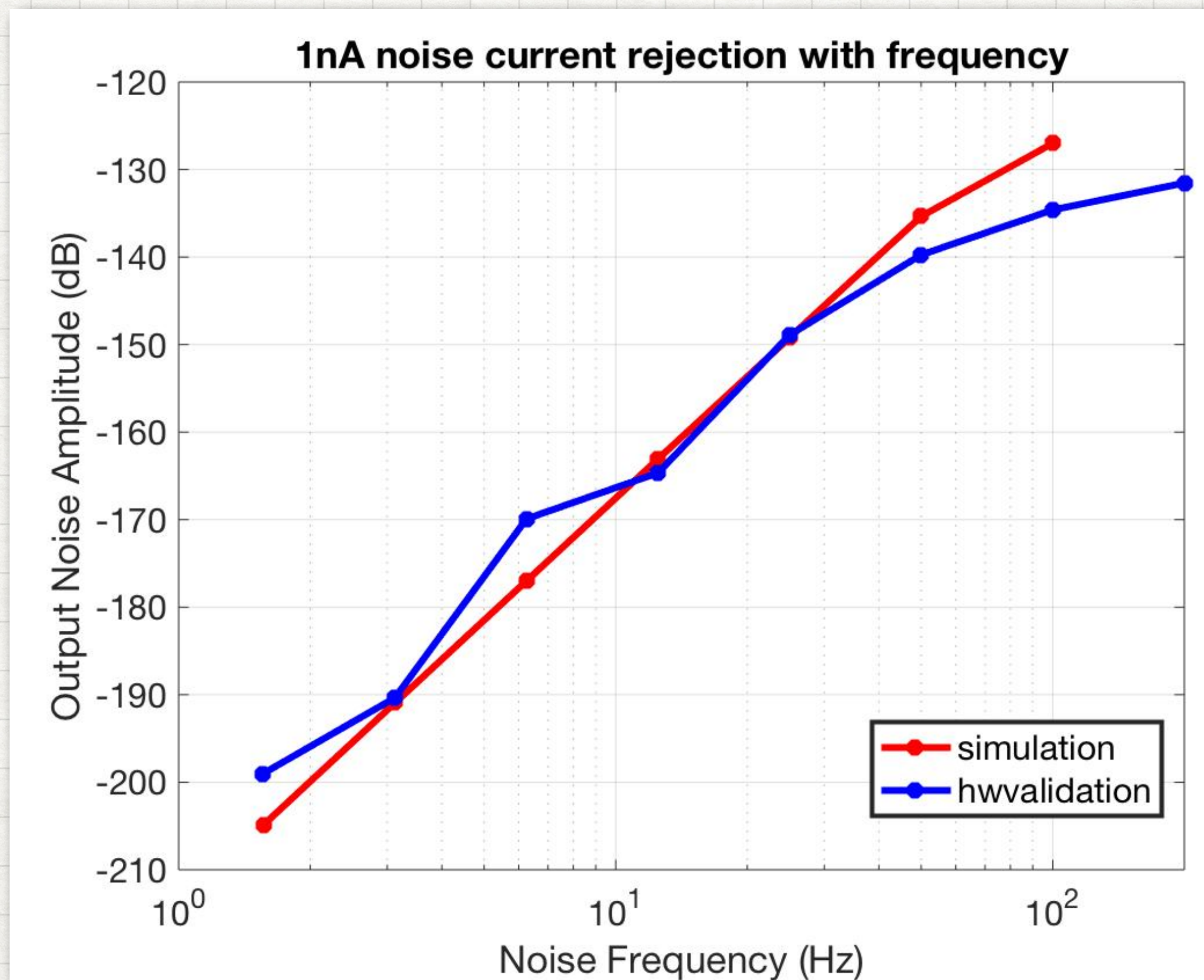


NOISE REJECTION SIMULATION RESULTS



HW VALIDATION

SLOPE MODULATOR





CONCLUSIONS



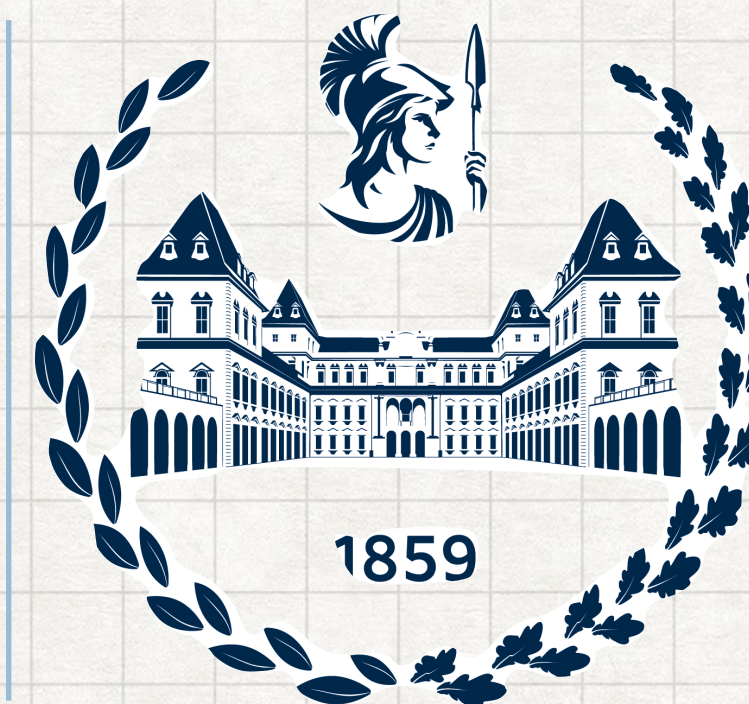
- Capacitive sensors: inconspicuous, low power, low cost, low maintenance
- Limitations:
 - Sensing range comparable to plate dimension
 - Environmental noise affects accuracy and sensing range
- Slope modulator can reject:
 - High frequency noise \rightarrow oversampling and decimation, low pass filter
 - Low frequency noise \rightarrow differential measurement technique

THANK YOU FOR THE ATTENTION

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